APPLICATION FOR U.S. LETTERS PATENT

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Entitled:

LITHIUM METAL OXIDE **ELECTRODES FOR LITHIUM BATTERIES**

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LITHIUM METAL OXIDE ELECTRODES FOR LITHIUM BATTERIES

CONTRACTUAL ORIGIN OF THE INVENTION

The United States Government has rights in this invention pursuant to Contract No. W-31-109-ENG-38 between the U.S. Department of Energy and The University of Chicago representing Argonne National Laboratory.

RELATED APPLICATION

This application, pursuant to 37 C.F.R. 1.78(c), claims priority based on co-pending U.S. Provisional Application Serial No. 60/465,034 filed on April 24, 2003.

FIELD OF THE INVENTION

This invention relates to improved lithium-metal-oxide positive electrodes for lithium cells and batteries, preferably rechargeable lithium-ion cells and batteries. These batteries are used to power a wide range of applications such as portable telecommunications equipment, computers, medical devices, electric vehicles and hybrid-electric vehicles. More specifically, the invention relates to lithium-metal-oxide electrodes with layered-type structures that are chemically preconditioned prior to cell assembly to improve the capacity, cycling efficiency and stability of lithium cells and batteries when charged to high potentials.

BACKGROUND OF THE INVENTION

State-of-the-art lithium-ion cells have a lithiated carbon negative electrode, or anode, (Li_xC_6) and a lithium-cobalt-oxide positive electrode, or cathode, $\text{Li}_{1-x}\text{CoO}_2$. During charge and discharge of the cells, lithium ions are transported between the two host structures of the anode and cathode with the simultaneous oxidation or reduction of the host electrodes, respectively. When graphite is used as the anode, the voltage of the cell is approximately 4 V. The LiCoO₂ cathode,

which has a layered structure, is expensive and becomes unstable at low lithium content, i.e., when cells reach an overcharged state at $x \ge 0.5$. Alternative, less expensive electrode materials that are isostructural with LiCoO₂, such as LiNi_{0.8}Co_{0.2}O₂, LiNi_{0.5}Mn_{0.5}O₂ and LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ are being developed with the hope of replacing at least part of the cobalt component of the electrode. However, all these layered structures, when extensively delithiated become unstable, because of the high oxygen activity at the surface of the particles. Therefore, the delithiated electrode particles tend to react with the organic solvents of the electrolyte or lose oxygen. Such reactions at the surface of layered lithium metal oxide electrodes are detrimental to the performance of the lithium cells and batteries, and methods are required to combat these reactions to ensure that maximum capacity and cycle life can be obtained from the cells.

Considerable efforts have already been made in the past to overcome the stability and solubility problems associated with layered LiCoO₂ and LiNiO₂ electrodes. For example, considerable success has been achieved in the past by stabilizing these electrodes by pre-treating the electrode powders with oxide additives such as Al₂O₃ or ZrO₂ obtained from metal alkoxide precursors such as solutions containing aluminum ethylhexanoate diisopropoxide (Al(OOC₈H₁₅)₂(OCH₃H₇)₂ or zirconium ethylhexanoisopropoxide (Zr[(OOC₈H₁₅)₂(OCH₃H₇)₂]) as described, for example, by J. Cho et al in Chemistry of Materials, Volume 12, page 3788 (2000) and J. Cho et al in Electrochemical and Solid State Letters, Volume 4 No. 10, page Al59 (2001), respectively, or a zirconium oxide, polymeric precursor or zirconium oxynitrate (ZrO(NO₃)₂•xH₂O) as described by Z. Chen et al in Electrochemical and Solid State Letters, Volume 5, No. 10, page A213 (2002), prior to the fabrication of the final electrode thereby making the surface of the LiCoO₂ particles more resistant to electrolyte attack, cobalt dissolution or oxygen loss effects.

The loss of oxygen from lithium metal oxide electrodes, such as layered LiCoO₂ and LiNi₁. $_y$ Co $_y$ O₂ electrodes can contribute to exothermic reactions with the electrolyte and with the lithiated carbon negative electrode, and subsequently to thermal runaway if the temperature of the cell reaches a critical value. Although some success has been achieved in the past to improve the performance of lithium-ion cells by coating electrode particles, the coatings can themselves impede lithium diffusion in and out of the layered electrode structure during electrochemical discharge and charge. Further improvements in the composition of layered lithium-metal oxide electrodes, particularly at the surface of the electrodes, and in methods to manufacture them are still required to improve the overall performance and safety of lithium cells.

SUMMARY OF THE INVENTION

This invention relates to improved lithium-metal-oxide positive electrodes for lithium cells and batteries, preferably rechargeable lithium-ion cells and batteries. More specifically, it relates to layered lithium-metal-oxide electrodes, represented by the general formula $xLi_2M'O_3 \bullet (1-x)LiMO_2$ ($0 \le x < 1$) in which M' is one or more non-lithium metal ions with an average tetravalent oxidation state and in which M is two or more non-lithium metal ions with an average trivalent oxidation state that are chemically preconditioned prior to cell assembly either by reduction or by acid treatment, or a combination thereof, to improve the capacity, cycling efficiency and cycling stability of lithium cells and batteries when charged to high potentials. The invention extends to methods for synthesizing the preconditioned lithium-metal-oxide electrodes.

BRIEF DESCRIPTION OF THE DRAWINGS

The invention consists of certain novel features and a combination of parts hereinafter fully described, illustrated in the accompanying drawings, and particularly pointed out in the appended

claims, it being understood that various changes in the details may be made without departing from the spirit, or sacrificing any of the advantages of the present invention.

FIG. 1 illustrates the powder X-ray diffraction patterns of a) an untreated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode; b) a $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode treated with NH₃ at 250 °C; and c) a $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode treated with NH₃ at 350 °C;

FIG. 2 illustrates the electrochemical voltage profiles, at the 15^{th} cycle, of lithium cells, operated at room temperature (RT) between 4.6 and 2.0 V, with a) an untreated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode; and b) a NH_3 -treated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode;

FIG. 3 illustrates the electrochemical voltage profiles, at the 15th cycle, of lithium cells operated at 50 °C between 4.6 and 2.0 V, with a) an untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode; and b) a NH₃-treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode;

FIG. 4 illustrates plots of electrode capacity vs. cycle number of lithium cells, operated at room temperature (RT) between 4.45 and 2.5 V, with a) an untreated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode; and b) a NH_3 -treated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode;

FIG. 5 illustrates plots of electrode capacity vs. cycle number of lithium cells, operated at room temperature (RT) between 4.6 and 2.0 V, with a) an untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode; and b) a NH₃-treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode;

FIG. 6 illustrates plots of electrode capacity vs. cycle number of lithium cells, operated at 50 °C between 4.6 and 2.0 V, with a) an untreated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode; and b) a NH_3 -treated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode;

FIG. 7a illustrates cyclic voltammograms between 4.6 and 2.0 V vs. metallic lithium of an untreated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode;

FIG. 7b illustrates cyclic voltammograms between 4.6 and 2.0 V vs. metallic lithium of a $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode treated with NH₃ at 250 °C;

FIG. 7c illustrates cyclic voltammograms between 4.6 and 2.0 V vs. metallic lithium of a $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode treated with NH₃ at 350 °C,

FIG. 8 illustrates the powder X-ray diffraction pattern of a) a $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ composite electrode; b) a $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ composite electrode treated with NH₃ at 200 °C; c) a $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ composite electrode treated first with H₂O at room temperature and then with NH₃ at 200 °C; and d) a $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ composite electrode treated first with HNO₃ at room temperature and then with NH₃ at 200 °C;

FIG. 9a illustrates the first charge and discharge voltage profiles of a lithium cell, operated at room temperature, with a 0.3Li₂MnO₃•0.7LiMn_{0.5}Ni_{0.5}O₂ composite electrode;

FIG. 9b illustrates the first charge and discharge voltage profiles of a lithium cell, operated at room temperature, with a 0.3Li₂MnO₃•0.7LiMn_{0.5}Ni_{0.5}O₂ composite electrode treated with NH₃;

FIG. 9c illustrates the first charge and discharge voltage profiles of a lithium cell, operated at room temperature, with a $0.3 \text{Li}_2 \text{MnO}_3 \bullet 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ composite electrode treated with H₂O and NH₃;

FIG. 9d illustrates the first charge and discharge voltage profiles of a lithium cell, operated at room temperature, with a $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ composite electrode treated with HNO₃ and NH₃;

FIG. 10a illustrates a plot of electrode capacity vs. cycle number of a lithium cell, operated at room temperature between 4.6 and 2.0 V, with an untreated 0.3Li₂MnO₃•0.7LiMn_{0.5}Ni_{0.5}O₂ composite electrode;

FIG. 10b illustrates a plot of electrode capacity vs. cycle number of a lithium cell, operated at room temperature between 4.6 and 2.0 V, with a $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ composite electrode treated with NH₃;

FIG. 10c illustrates a plot of electrode capacity vs. cycle number of a lithium cell, operated at room temperature between 4.6 and 2.0 V, with a $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ composite electrode treated with H₂O and NH₃;

FIG. 10d illustrates a plot of electrode capacity vs. cycle number of a lithium cell, operated at room temperature between 4.6 and 2.0 V, with a $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ composite electrode treated with HNO₃ and NH₃;

FIG. 11 illustrates a schematic representation of an electrochemical cell; and

FIG. 12 illustrates a schematic representation of a battery consisting of a plurality of cells connected electrically in series and in parallel.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

It is now well known that state-of-the-art LiMO₂ electrodes with layered structures such as $LiCoO_2$, $LiNi_{0.8}Co_{0.2}O_2$, $LiAl_{0.05}Ni_{0.80}Co_{0.15}O_2$, $LiNi_{0.5}Mn_{0.5}O_2$, $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$, $LiNi_{0.80}Co_{0.15}Al_{0.05}O_2$ and $LiCo_{0.90}Ti_{0.05}Mg_{0.05}O_2$ electrodes, or variations thereof, for example, those that contain lithium within the transition metal (M) layers are unstable in a lithium cell environment when a large amount of lithium is extracted from their structures, typically when x exceeds 0.5 in $Li_{1.x}MO_2$ electrodes, or at a potential higher than approximately 4.2 V vs. metallic

lithium. The high reactivity of the delithiated electrode structure has been attributed to the highly oxidizing power of the tetravalent metal ions Ni^{4+} , Co^{4+} and Mn^{4+} , that decreases in the order $Ni^{4+} > Co^{4+} > Mn^{4+}$. Highly delithiated $Li_{1-x}MO_2$ electrodes can therefore react spontaneously with the organic-based electrolyte solvents such as ethylene carbonate, diethyl carbonate or dimethyl carbonate or, in extreme cases, the $Li_{1-x}MO_2$ electrode can release oxygen into the cell compartment. The oxidation of electrolyte solvents or the release of oxygen from the delithiated electrodes, which can be represented generically by the formula $Li_{1-x}MO_{2-\delta}$ (0< δ <1), must of necessity lower the oxidation state of the transition metal ions in the $Li_{1-x}MO_{2-\delta}$ product, at least at the surface of the electrode particles. Such a reaction takes place predominantly during the initial charge of a C_6 / $LiMO_2$ lithium-ion cell, when lithium is electrochemically extracted from the $LiMO_2$ positive electrode and inserted into the negative C_6 (graphite) electrode. These reactions decrease the theoretical capacity of the $LiMO_2$ electrode; therefore, these electrodes tend to show an enhanced capacity loss on the initial charge/discharge cycle of the lithium-ion cell.

For layered LiMO₂ electrodes that contain Ni, such as LiNiO₂, LiNi_{0.8}Co_{0.2}O₂ and LiAl_{0.05}Ni_{0.80}Co_{0.15}O₂, it has been observed that the electrochemically induced capacity loss can be attributed not only to oxygen loss or reaction with the electrolyte, but also to the migration of the nickel ions into the lithium layer of the delithiated Li_{1.x}MO_{2. δ} electrode structure. When nickel diffusion occurs concomitantly with oxygen loss, then the surface of a Li_{1.x}MO_{2. δ} electrode can have characteristic features, for example, of a Li₂M_{1.2}O rocksalt-like structure. For example, lithium extraction and oxygen loss from a Li_{1.x}NiO_{2. δ} electrode leaves a surface product that closely resembles a Li₂Ni_{1.2}O phase. Although a Li₂Ni_{1.2}O structure lowers the lithium-ion conductivity at the electrode surface, which can result in an increase in cell impedance, the reduced surface layer

serves to protect the Li_{1.x}MO₂ structure within the bulk of the particles during the extended cycling of the lithium-ion cell. The applicants have found that it is advantageous to pre-reduce chemically the surface of LiMO₂ electrode particles, particularly those containing a slight excess of lithium within the M layers, with a convenient reducing agent to yield a LiMO₂₋₈ electrode product prior to cell assembly so that the extent of oxygen loss from the electrode and the concomitant loss of capacity could be minimized during the electrochemical charge and discharge of the cell. In this respect, the use of reducing environments to synthesize electrode products has already been disclosed in the literature for different types of electrodes as discussed by M. M. Thackeray et al in U.S. Patent 5,240,794; in these instances the reduced metal ions exist in the bulk of the electrode structures as well as at the surface of the particles.

Layered lithium-metal-oxide structures, Li₂M'O₃, in which the M' ions are tetravalent, are also known to exist. These structures can be reformulated in standard layered notation as Li[M'_{0.67}Li_{0.33}]O₂ in which layers of lithium ions alternate with layers containing both M'- and lithium ions in a 2:1 ratio. One well known example is Li₂MnO₃ (Li[Mn_{0.67}Li_{0.33}]O₂) which is electrochemically inactive with respect to lithium insertion and extraction. However, Li₂MnO₃ can be electrochemically activated by acid treatment, during which some H⁺-Li⁺ ion exchange occurs and some Li₂O may be removed from the structure.

This invention relates, in general, to layered lithium-metal-oxide electrodes, represented by the general formula $xLi_2M'O_3 \bullet (1-x)LiMO_2$ ($0 \le x < 1$) in which M' is one or more non-lithium metal ions with an average tetravalent oxidation state and in which M is one or more non-lithium metal ions with an average trivalent oxidation state that are chemically preconditioned prior to cell assembly either by reduction or by acid treatment, or a combination thereof, to improve the

capacity, cycling efficiency and cycling stability of lithium cells and batteries when charged to high potentials. The invention extends to methods for synthesizing the preconditioned lithium-metal-oxide electrodes. When x=0, the formula $xLi_2M'O_3 \bullet (1-x)LiMO_2$ reduces simply to $LiMO_2$.

Therefore, in a first embodiment, this invention relates to layered electrodes represented by the two-component formula $x \text{Li}_2 M' O_3 \bullet (1-x) \text{Li} M O_2$ in which $0 \le x < 1$, that can be rewritten alternatively as $\text{Li}_{(2+2x)/(2+x)}M'_{2x/(2+x)}M'_{(2-2x)/(2+x)}O_2$ also for $0 \le x < 1$, in which M is a non-lithium metal ion with an average trivalent oxidation state selected from one or more of the first row transition metals or lighter metal elements in the periodic table, and in which M' is one or more ions with an average tetravalent oxidation state selected from the first and second row transition metal elements and Sn, the electrodes being chemically preconditioned with a reducing agent to yield $\text{Li}_{(2+2x)\!/(2+x)} M'_{2x/(2+x)} M_{(2-2x)\!/(2+x)} O_{2-\delta} \text{ compounds in which } \delta \text{ is less than } 0.2, \text{ preferably less than } 0.1.$ The metal ions, M, are selected preferably from Co, Ni, Mn or Ti ions, optionally in the presence of one or more other cations such as Mg and Al. The M' cations are selected from elements that form a Li₂M'O₃ rocksalt-type structure preferably from Ti, Mn, Zr, Ru and Sn and most preferably from Mn and/or Ti that form a layered rocksalt-type structure which is structurally compatible with the LiMO₂ component. The xLi₂M'O₃•(1-x)LiMO₂ electrodes have been described previously as having composite electrode structures by J-S. Kim et al in Electrochemistry Communications, volume 4, page 205 (2002). When x=0, the preconditioned electrodes are represented simply by the formula LiMO_{2-δ}.

In a second embodiment of the invention, the $xLi_2M'O_3 \bullet (1-x)LiMO_2$ electrodes can be preconditioned by acid treatment optionally followed by the reduction step. When preconditioning occurs by acid treatment, ion-exchange occurs between the H^+ and Li^+ ions. In this instance, the

preconditioned $xLi_2M'O_3 \bullet (1-x)LiMO_2$ electrodes can be represented prior to reduction by the general formula $xLi_{2-y}H_yO \bullet xM'O_2 \bullet (1-x)Li_{1-z}H_zMO_2$ in which 0 < x < 1, 0 < y < 1, 0 < z < 1, and in which the lithium ions are partially ion-exchanged by hydrogen ions. In addition, some Li_2O may be removed from the structure during this process. These preconditioned electrodes can be heated, typically to temperatures above 100 °C, to remove at least part of the H_2O component from the structure.

Of particular significance to this invention are preconditioned xLi₂M'O₃•(1-x)LiMO₂ electrodes containing a Li₂MnO₃ component (i.e., M'=Mn). It has already been reported by M. H. Rossouw et al in the Journal of Solid State Chemistry, volume 104, page 464 (1993) that lithium and oxygen can be removed from Li₂MnO₃ by acid treatment to create a composite xLi₂MnO₃·(1x)MnO₂ structure without destroying the layered arrangement of the Mn ions; on relithiation, either chemically with LiI or electrochemically in an electrochemical cell, lithium can be inserted into the MnO₂ component of the composite structure to yield xLi₂MnO₃•(1-x)LiMnO₂. These composite electrode structures may contain protons (H⁺ ions) as a result of the H⁺ - Li⁺ ion exchange reactions that occur, for example, during the preconditioning acid-treatment step or when immersed in the non-aqueous electrochemical cells that contain acidic electrolytes such as those containing LiPF₆ salts. For simplicity, these protons are not always included in the description of the preconditioned electrode structures of this invention. The composition of xLi₂MnO₃•(1-x)LiMO₂ electrodes can be modified by selection of one or more appropriate metal (M) cations, preferably from one or more of Co, Ni, Mn or Ti, ions, optionally in the presence of one or more other metal cations, selected preferably from the first row of transition metal elements, or from lighter metal elements in the periodic table, such as Mg and Al. Examples of such two-component systems are

 $xLi_2MnO_3 \bullet (1-x)LiCoO_2$ as reported by K. Numata et al in Solid State Ionics, volume 118, page 117 (1999), and $xLi_2MnO_3 \bullet (1-x)LiCrO_2$ as reported by B. Ammundsen et al in the Journal of the Electrochemical Society, volume 149, page A431 (2002). Composite electrodes that are showing particular promise typically contain two or more electrochemically-active M cations, for example, $Li[Ni_xLi_{(1/3-2x/3)}Mn_{(2/3-x/3)}]O_2$ (0<x<1/2) as reported by Z. Lu et al in Chemistry of Materials, volume 15, page 3214 (2003), which can be reformulated in composite notation as (1-2x) $Li_2MnO_3 \bullet (3x)LiMn_{0.5}Ni_{0.5}O_2$ for the same range of x, and electrodes in which M=Co, Mn and Ni, represented generically as $xLi_2MnO_3 \bullet (1-x)LiCo_{1-a}Ni_bMn_cO_2$ in which a=b+c.

A major advantage of using two-component xLi₂M'O₃•(1-x)LiMO₂ composite (positive) electrodes, as defined herein, is that the Li₂M'O₃ component, particularly when present as Li₂MnO₃, can be used effectively to supply an excess of lithium to the positive electrode to offset irreversible capacity loss effects associated with the negative electrode of lithium-ion cells, such as lithiated graphite, Li_xC₆ (0<x<1). For example, it has been established that when xLi₂MnO₃•(1-x)LiNi_{0.3}Mn_{0.3}O₂ electrodes are charged in lithium cells, the electrochemical reaction occurs first by lithium extraction from the LiNi_{0.3}Mn_{0.3}O₂ component between 3.0 and 4.2 V, and thereafter by a concomitant extraction of lithium from the Li₂MnO₃ component. It is believed that the latter process (typically at potentials between 4.2 and 4.6 V) is also accompanied by the chemical loss of oxygen from the surface of the delithiated xLi₂MnO₃•(1-x)LiNi_{0.3}Mn_{0.3}O₂ electrode particles, either as oxygen gas or by reaction with the organic solvents of the electrolyte, for example, organic carbonates such as ethylene carbonate, dimethyl carbonate, diethyl carbonate and the like. In such situations, the result is not only a chemical reduction of the electrode surface by loss of oxygen, but also the loss of some Li₂O from the Li₂MnO₃ (Li₂O•MnO₃) component that leaves behind an

electrochemically active MnO_2 species, thereby increasing the operating capacity of the electrode. Despite the fact that $xLi_2M'O_3 \bullet (1-x)LiMO_2$ composite electrodes exhibit an irreversible capacity loss during the initial cycle, these electrodes provide significantly higher electrode capacities on subsequent cycling than conventional layered $LiCoO_2$ or $LiNiO_2$ electrodes and $LiMn_2O_4$ spinel electrodes. It would be advantageous to precondition layered $LiMO_2$ or composite $xLi_2M'O_3 \bullet (1-x)LiMO_2$ electrodes chemically prior to assembling them in cells by removing oxygen and/or Li_2O from the surface of the electrodes to minimize irreversible capacity loss effects and to increase the operating capacity of the electrodes, particularly during the early cycling of cells.

According to a third embodiment, the preconditioned electrodes of the invention can be synthesized by subjecting the parent LiMO₂ or composite xLi₂M'O₃•(1-x)LiMO₂ electrodes, for example, either in powder or laminate form, to a suitable reducing agent such as ammonia gas, dilute hydrogen gas, for example, 2-6 percent by volume of hydrogen in argon gas, carbon monoxide gas, or carbon at moderately high temperatures, such as 150 - 600 °C, to reduce the surface of the LiMO₂ or composite xLi₂M'O₃•(1-x)LiMO₂ electrodes. Gaseous reducing agents, such as ammonia, are preferred to solid reducing agents such as finely-divided carbon powder because it is easier to control the extent to which the surface of the LiMO₂ electrode is reduced. Alternatively, the LiMO₂ or composite xLi₂M'O₃•(1-x)LiMO₂ electrodes can be reduced by heating the electrodes under nitrogen gas or air at elevated temperature, typically at 600 °C or higher, for example, between 900 °C and 1000 °C simultaneously to remove both oxygen and Li₂O from the surface of the electrode structure.

In a further embodiment of the invention, the LiMO₂ or xLi₂M'O₃•(1-x)LiMO₂ composite electrodes of the invention can alternatively be subjected, prior to the reduction process described

above, to a preconditioning step in a proton-containing medium, for example, de-ionized water or an acidic solution with a pH<7.0 such as nitric acid, acetic acid, hydrochloric acid or the like, to exchange some of the Li⁺ ions within the electrode structure with H⁺ ions, and thereafter to a heating step, preferably for less than 24 hours below 500 °C, more preferably below 400 °C. In yet a further embodiment, the LiMO₂ or xLi₂M'O₃•(1-x)LiMO₂ composite electrodes may be preconditioned by subjecting the electrodes only to the proton-containing medium, i.e., without a reduction step. For example, it is already known that acid treatment of Li₂MnO₃ yields a proton-exchanged Li_{2-y}H_yMnO₃ compound that can be reformulated, in component notation, as (1-y/2)Li₂O•y/2H₂O•MnO₂. It is believed that such an ion-exchange process followed by a heat-treatment step may be used effectively to precondition the electrode because it should be easier to remove (or partially remove), by heating, a H₂O component from the structure rather than a Li₂O component, in order to increase the MnO₂ component in the initial electrode and therefore its inherent electrochemical capacity.

In a final embodiment, this invention extends to include electrochemical lithium cells and batteries that employ the preconditioned $LiMO_2$ or composite $xLi_2M'O_3 \bullet (1-x)MO_2$ electrodes as fully described herein.

The following examples describe the principles of the invention and possible methods of synthesizing the pre-reduced electrodes of this invention as contemplated by the inventors, but they are not to be construed as limiting examples.

EXAMPLE 1

Synthesis of $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrodes

 $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2 \ powder \ was \ synthesized \ from \ LiOH \bullet H_2O \ and \ Mn_{0.33}Ni_{0.33}Co_{0.33}(OH)_x$ LiOH•H₂O was used as supplied by Aldrich (98% pure). $(x\sim2)$ precursors. The Mn_{0.33}Ni_{0.33}Co_{0.33}(OH)_x precursor was prepared by coprecipitation of the required stiochiometric amounts of metal nitrates M(NO₃)₂•xH₂O (M=Mn, Ni, and Co). After intimate mixing and grinding, the powdered mixture was pressed into a pellet and placed in a muffle furnace. A twostep heating procedure was used to fire the pellet according to the following procedure. First, a low temperature calcination step was performed at 480 °C for 5 hr. The pellet was then ground again and recompacted into pellet form. Second, a high temperature sintering step was performed at 900 °C for 3 hr followed by rapid quenching of the pellet between two copper plates. The pellet was ground a final time. Samples of the resulting LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ powder were heated at either 250 or 350 °C for approximately 20 hr in a tubular furnace under flowing NH₃ gas. The X-ray diffraction patterns of the parent LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ compound and the NH₃-treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ samples are shown in Figure 1(a-c), respectively; there were no significant differences in the X-ray patterns of the untreated- and NH3-treated LiMn $_{0.33}$ Ni $_{0.33}$ Co $_{0.33}$ O $_2$ sample, indicating that there were no substantial changes to the bulk of the electrode structure.

EXAMPLE 2

Electrochemical evaluation of LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrodes

Electrochemical evaluation of $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ and preconditioned $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ positive electrodes was carried out as follows. The electrodes for the lithium cell were fabricated from an intimate mixture of 84 wt% of $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode powder,

8 wt% polyvinylidene difluoride (PVDF) polymer binder (Kynar, Elf-Atochem), 4 wt% acetylene black (Cabot), and 4 wt% graphite (SFG-6, Timcal) slurried in 1-methyl-2-pyrrolidinone (NMP) (Aldrich, 99+%). An electrode laminate was cast from the slurry onto an Al current collector foil using a doctor-blade. The laminate was subsequently dried, first at 75°C for 10 h, and thereafter under vacuum at 70°C for 12 h. The electrolyte was 1 *M* LiPF₆ in ethylene carbonate (EC):diethyl carbonate (DEC) (1:1 mixture). The electrodes were evaluated at both room temperature and 50 °C in coin-type cells (size CR2032, Hohsen) with a lithium foil counter electrode (FMC Corporation, Lithium Division) and a polypropylene separator (Celgard 2400). Cells were assembled inside a He glovebox (<5 ppm, H₂O and O₂) and cycled on a Maccor Series 2000 tester under galvanostatic mode with a constant current density of either 0.3 mA/cm² or 0.1 mA/cm².

The electrochemical voltage profiles, at the 15^{th} cycle, of lithium cells, operated at room temperature between 4.6 and 2.0 V, with an untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode and a NH₃-treated (250 °C) LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode are shown in Figure 2 (a and b), respectively. It is clearly apparent that the capacity delivered by the electrochemical cell containing the NH₃-treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode is significantly superior to that of the cell with the untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode in accordance with the principles of the invention.

The electrochemical voltage profiles, at the 15th cycle, of lithium cells, operated at 50 °C between 4.6 and 2.0 V, with an untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode and a NH₃-treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode are shown in Figure 3 (a and b), respectively. It is clearly apparent that the capacity delivered by the electrochemical cell containing the NH₃-treated (250 °C) LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode is significantly superior to that of the cell with the untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode in accordance with the principles of the invention. Figure 4 (a and

b) represents plots of electrode capacity vs. cycle number of lithium cells operated at room temperature between 4.6 and 2.0 V, with an untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode and a NH₃treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode, respectively, whereas Figure 5 (a and b) represents plots of electrode capacity vs. cycle number of lithium cells operated at room temperature between 4.45 and 2.5 V, with an untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode and a NH₃-treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode, respectively. Figure 6 (a and b) represents plots of electrode capacity vs. cycle number of lithium cells operated at 50 °C, between 4.6 and 2.0 V, with an untreated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode and a NH_3 -treated $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrode, respectively. These data clearly illustrate the superior capacity delivered consistently by the NH₃ $treated\ LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2\ electrodes\ compared\ to\ the\ untreated\ LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2\ electrodes$ in accordance with the principles of this invention. Of particular note is that the coulombic efficiency of the cells containing the NH₃-treated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode is notably superior to that of the cell containing the untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode (Figures 4 and 5). The NH₃ preconditioning step also increases the first-cycle reversible capacity of the LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrodes from 83% (unconditioned electrode, Sample A) to 88% (preconditioned electrodes, Samples B and C) as shown in Table 1.

Table 1. Charge/discharge capacities and reversible capacity (%) of the initial cycle of lithium cells with unconditioned- and preconditioned $LiMn_{0.33}Ni_{0.33}Co_{0.33}O_2$ electrodes.

Electrode	Initial Charge Capacity	Initial Discharge	Reversible Capacity
	(mAh/g)	Capacity (mAh/g)	(%)
Sample A	229	191	83
Sample B	228	200	88
Sample C	229	201	88

Figures 7a, 7b and 7c (samples A-C, respectively) represent plots of cyclic voltammograms between 4.6 and 2.0 V vs. metallic lithium of an untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode, a LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode treated with NH₃ at 250 °C, and a LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode treated with NH₃ at 350 °C, respectively. It is significant that the second oxidative sweep of the untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode between 3.5 and 4.25 V (Figure 7a) occurs at a lower potential than the initial sweep, indicating that the surface of the electrode had been reduced electrochemically during the first cycle. By contrast, the difference in potential between the first and second oxidative sweep of an LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode treated with NH₃ at 250 °C (Figure 7b) and at 350 °C (Figure 7c) is less than it is for the untreated LiMn_{0.33}Ni_{0.33}Co_{0.33}O₂ electrode (Figure 7a), consistent with the principles of the invention that NH₃ treatment reduces the electrode surface to provide enhanced electrode stability as demonstrated by the improved

coulombic efficiency of the NH₃-treated electrodes (Figs. 4 and 5). These data illustrate that preconditioning the electrode produces improved cycling characteristics. Although it is difficult to determine the precise degree to which the parent electrode is reduced by the chemical preconditioning process, particularly at the surface, excessive reduction will damage the electrode structure and degrade the electrochemical properties of the electrode. It is therefore, believed that optimum electrochemical performance will only be achieved for mild levels of reduction, i.e., for δ less than 0.2, preferably less than 0.1 in the $\text{Li}_{(2+2x)/(2+x)}M'_{2x/(2+x)}M_{(2-2x)/(2+x)}O_{2-\delta}$ electrodes of this invention.

EXAMPLE 3

Synthesis of $0.3Li_2MnO_3 \cdot 0.7LiMn_{0.5}Ni_{0.5}O_2$ composite electrodes

An electrode material with the composite formula $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ was prepared directly from Ni_{1-x}Mn_x(OH)₂ and LiOH•H₂O precursors using the required Li:Mn:Ni ratio. The Ni_{1-x}Mn_x(OH)₂ precursor was prepared by precipitation from a basic LiOH solution of Ni(NO₃)₂ and Mn(NO₃)₂ (pH ~ 11). The reagents were intimately mixed in an acetone slurry, dried in an oven overnight, and subsequently fired at 480 °C for 12 h and then at 900 °C for 5 h in air. Thereafter, the $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ product was rapidly quenched (also in air). The X-ray diffraction pattern of the resulting powder is shown in Fig. 8a (Sample D). The electrode powder was preconditioned according to the following procedures prior to cell assembly: 1) subjecting the powder to flowing NH₃ gas in a tubular furnace at 200 °C for approximately 20 hrs, the X-ray diffraction pattern of this product being shown in Fig. 8b (Sample E); 2) washing the powder in de-ionized water (pH ~6.5) before subjecting the powder to flowing NH₃ gas in a tubular furnace at 200 °C for approximately 20 hrs, the X-ray diffraction pattern of this product

being shown in Fig. 8c (Sample F); 3) treating the powder with 0.1M HNO₃ (pH ~1.8) before subjecting the powder to flowing NH₃ gas in a tubular furnace at 200 °C for approximately 20 hrs, the X-ray diffraction pattern of this product being shown in Fig. 8d (Sample G). There were no significant differences in the X-ray patterns of Samples D, E, F and G, indicating that there were no significant changes to the bulk structure of the individual compounds. Refinement of the lattice parameters of Samples D, E and G using rhombohedral symmetry (hexagonal setting), which is typical of layered-type compounds such as $LiCoO_2$ (Table 2), showed that there was an insignificant change of the lattice parameters after NH₃-treatment (Sample D). However, the slight expansion of the c-axis in Sample G is consistent with the removal of some lithium from the composite structure as a result of acid-treatment.

Table 2. Lattice parameters of Samples D, E, and G.

Electrode	a (Å)	c (Å)
Sample D (untreated)	2.8655(3)	14.254(3)
Sample E (NH ₃ -treated)	2.8666(3)	14.259(3)
Sample G (HNO ₃ /NH ₃ -treated)	2.8711(3)	14.271(4)

EXAMPLE 4

Electrochemical evaluation of $0.3Li_2MnO_3 \cdot 0.7LiMn_{0.5}Ni_{0.5}O_2$ composite electrodes

The construction of lithium cells containing $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ and preconditioned $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ positive electrodes was carried out by the same

procedure as described in Example 2. Cells were cycled under galvanostatic mode between 4.6 and 2.0 V at constant current density (0.1 mA/cm²).

The voltage profiles of the first charge/discharge cycle of lithium cells with: an untreated $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ electrode (Sample D); an NH₃-treated $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ electrode (Sample E); an H₂O/NH₃-treated $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ electrode (Sample F); and an HNO₃/NH₃-treated $0.3\text{Li}_2\text{MnO}_3 \cdot 0.7\text{LiMn}_{0.5}\text{Ni}_{0.5}\text{O}_2$ electrode (Sample G) are shown in Fig. 9(a-d), respectively. The capacities obtained during the first charge and discharge and the cycling efficiency of the initial cycle of these cells are provided in Table 2 and illustrated graphically in Fig. 10(a-d), respectively.

Table 3. Charge/discharge capacities and reversible capacity (%) of the initial cycle of lithium cells with $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ and preconditioned $0.3 \text{Li}_2 \text{MnO}_3 \cdot 0.7 \text{LiMn}_{0.5} \text{Ni}_{0.5} \text{O}_2$ electrodes.

Electrode	Initial Charge	Initial Discharge	Reversible Capacity
	Capacity (mAh/g)	Capacity (mAh/g)	(%)
Sample D	259	203	78
Sample E	254	199	78
Sample F	248	204	82
Sample G	205	195	95

The data in Table 3 demonstrate that an improvement in the irreversible capacity loss during the initial cycle can be obtained by preconditioning xLi₂M'O₃•(1-x)LiMO₂ composite electrodes, particularly those containing a Li₂MnO₃ component by subjecting the electrodes to an acidic medium, e.g., deionized water (pH ~6.5) or an HNO₃ solution (pH ~1.8) and that the improvement is significantly more pronounced when the electrodes are preconditioned with acid at low pH (Sample G, 95% efficiency). The excellent 95% capacity retention of electrode sample G when charged to the high potential of 4.6 V vs. Li⁰ is indicative of a stabilized electrode with a significantly reduced surface reactivity compared with electrode samples D, E and F.

The examples and results of this invention demonstrate that improved electrochemical performance of a layered lithium metal oxide electrodes as defined herein, can be significantly improved by preconditioning the electrodes either with a reducing agent such as ammonia or by acid treatment or a combination thereof, particularly when the electrodes are subjected to high potentials in excess of 4.2 V during charge. This invention, therefore, also relates to non-aqueous electrochemical lithium cells containing such preconditioned positive electrodes, a typical cell shown schematically in Figure 11, represented by the numeral 10 having a negative electrode 12 separated from a positive electrode 16 by an electrolyte 14, all contained in an insulating housing 18 with suitable terminals (not shown) being provided in electronic contact with the negative electrode 12 and the positive electrode 16. Binders and other materials normally associated with both the electrolyte and the negative and positive electrodes are well known in the art and are not fully described herein, but are included as is understood by those of ordinary skill in this art. Figure 12 shows a schematic illustration of one example of a battery in which two strings of electrochemical lithium cells, described above, are arranged in parallel, each string comprising

three cells arranged in series. The invention also includes methods of making the preconditioned positive electrodes, cells and batteries including same.

While there has been disclosed what is considered to be the preferred embodiments of the present invention, it is understood that various changes in the details may be made without departing from the spirit, or sacrificing any of the advantages of the present invention and that additional improvements in the capacity and stability of the electrodes can be expected to be made in the future by improving and optimizing the processing techniques whereby lithium metal oxide electrodes are chemically preconditioned either by acid treatment or reduction processes, or a combination thereof, prior to the construction of electrochemical lithium cells.